

CHAPTER 7

HYDRAULIC ACTUATORS



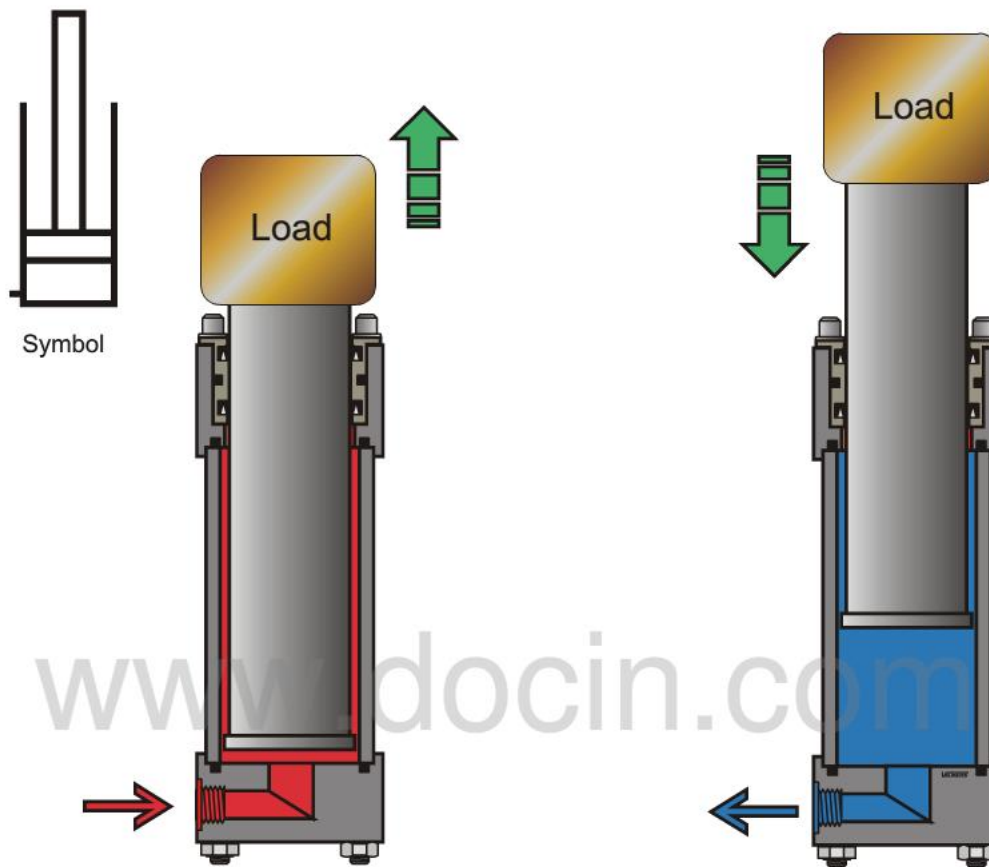


Figure 7-1 Ram Cylinder

COPYRIGHT © (2001) EATON CORPORATION

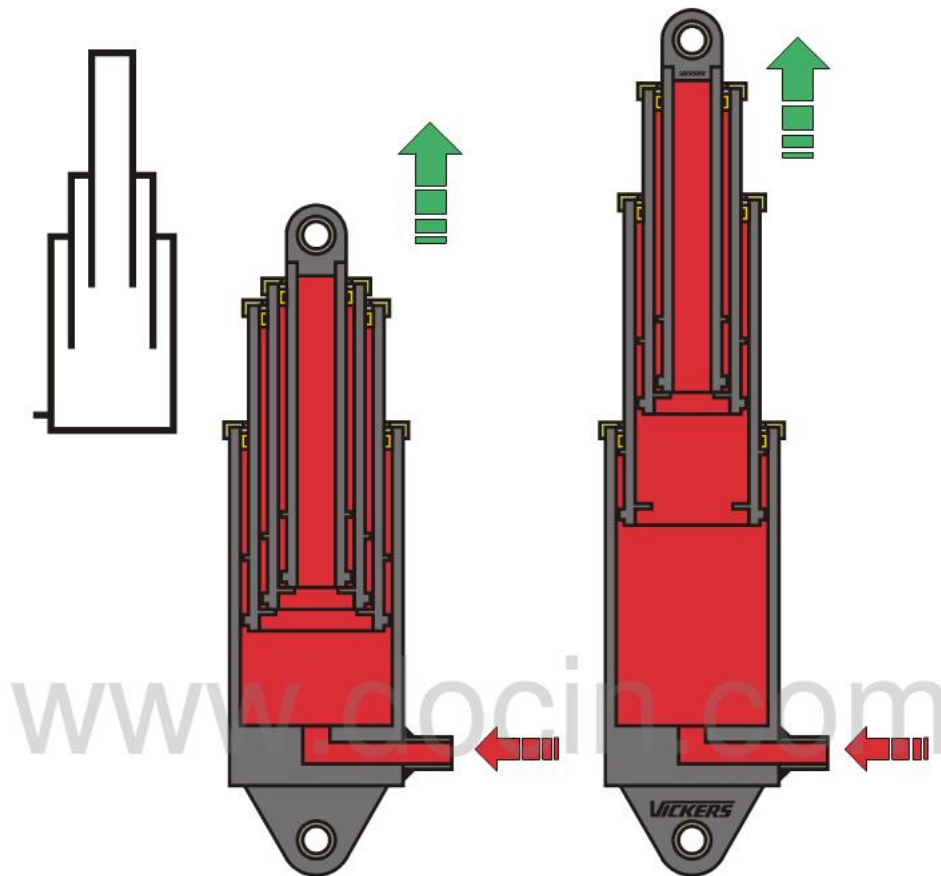


Figure 7-2 Single acting telescope cylinder

COPYRIGHT © (2001) EATON CORPORATION

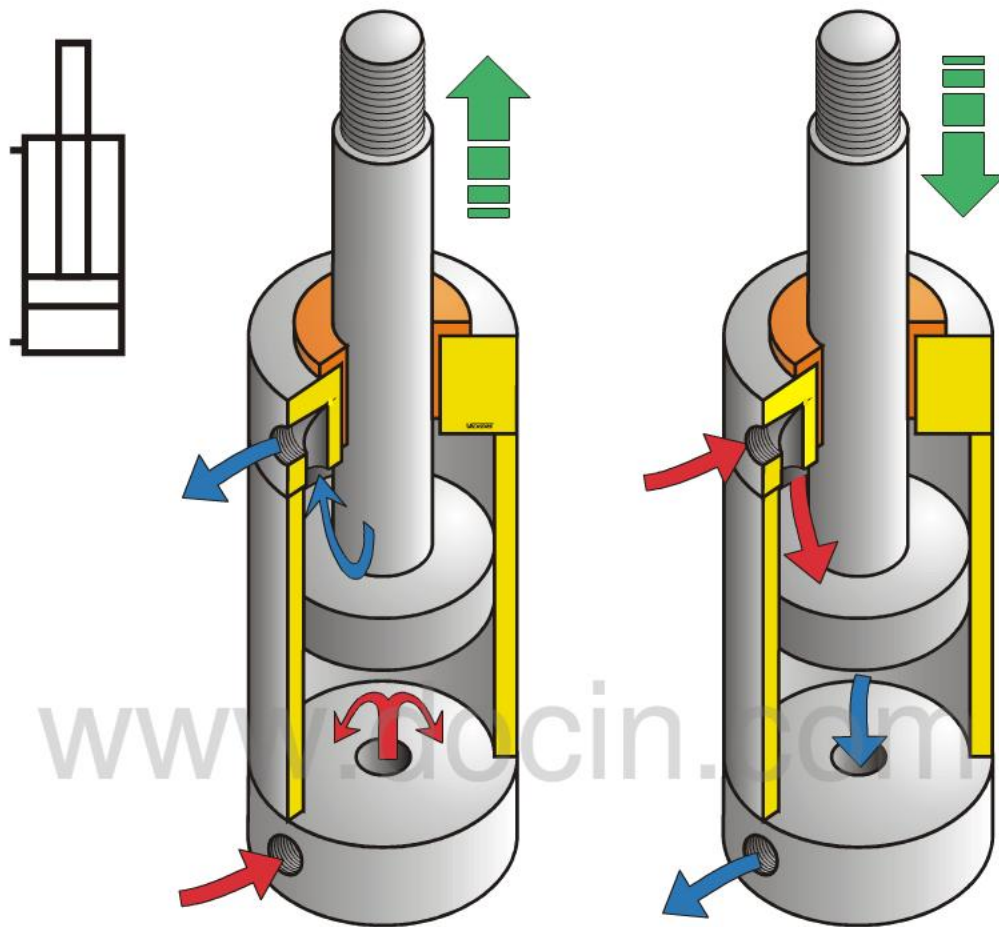


Figure 7-3 Basic double acting cylinder

COPYRIGHT © (2001) EATON CORPORATION

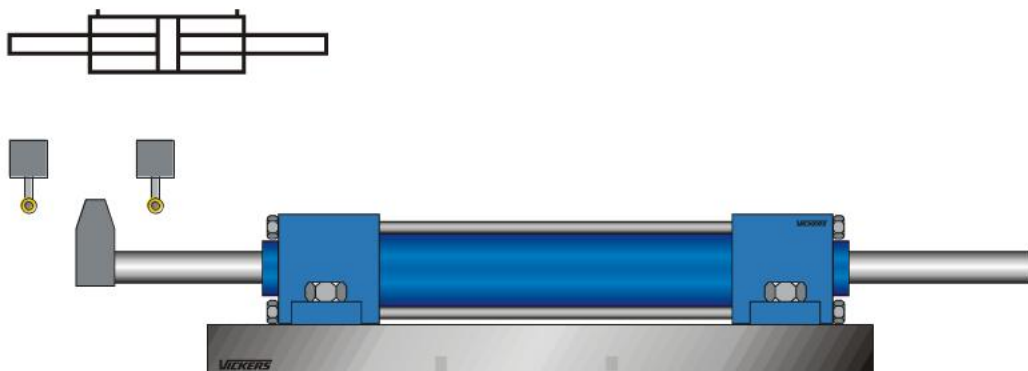


Figure 7-4 Double rod cylinder

COPYRIGHT © (2001) EATON CORPORATION

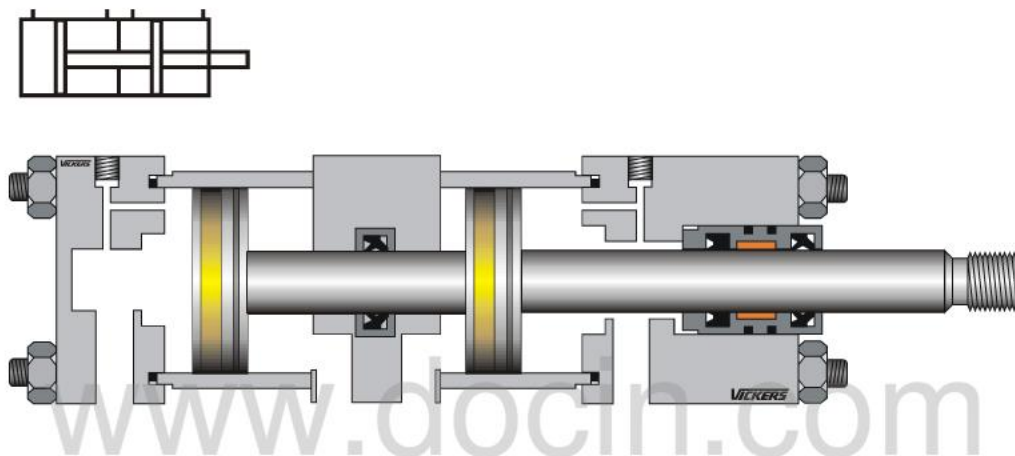


Figure 7-5 Tandem cylinder

COPYRIGHT © (2001) EATON COPORATION

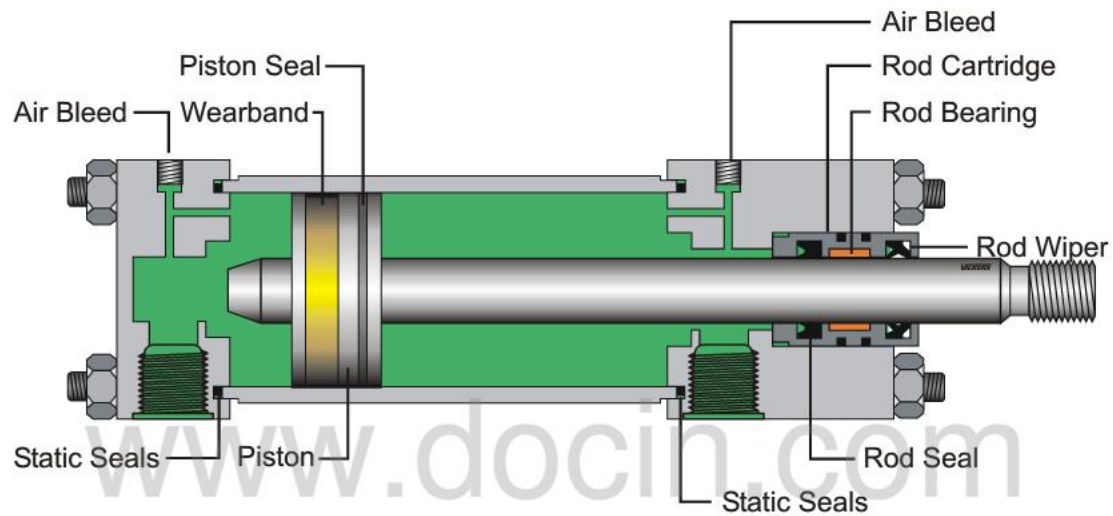


Figure 7-6 Typical cylinder construction

COPYRIGHT © (2001) EATON CORPORATION

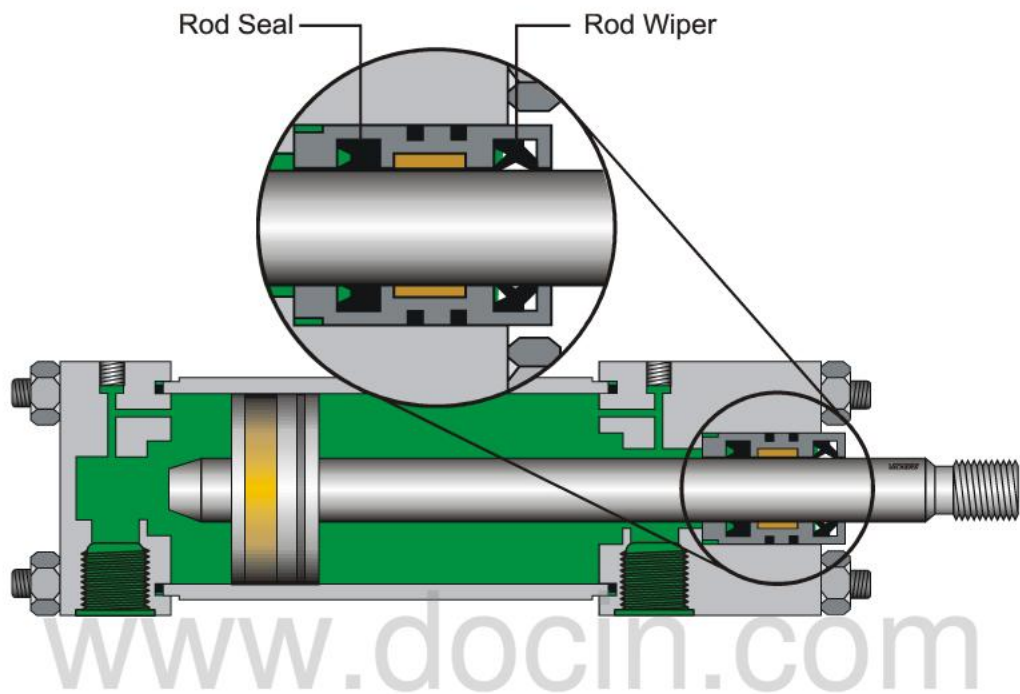


Figure 7-7 Rod seal and wiper design

COPYRIGHT © (2001) EATON CORPORATION

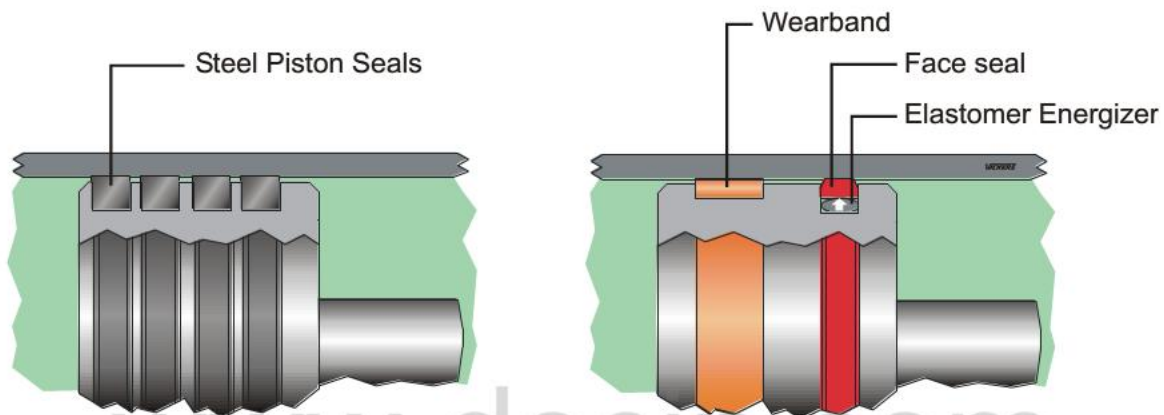


Figure 7-8 Metal sealing rings

COPYRIGHT © (2001) EATON CORPORATION

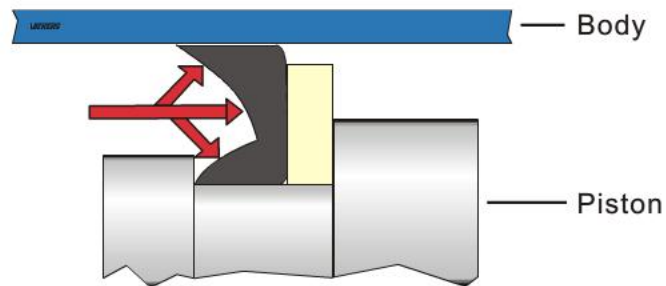
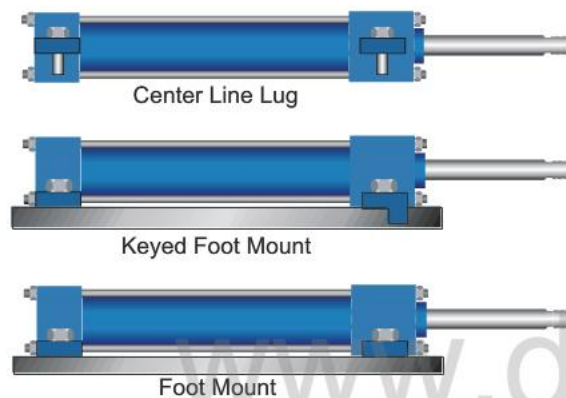


Figure7-9 Pressure tightens the seal to improve sealing

COPYRIGHT © (2001) EATON CORPORATION

Lug and Foot Mounts



Extended Tie Rod Mounts

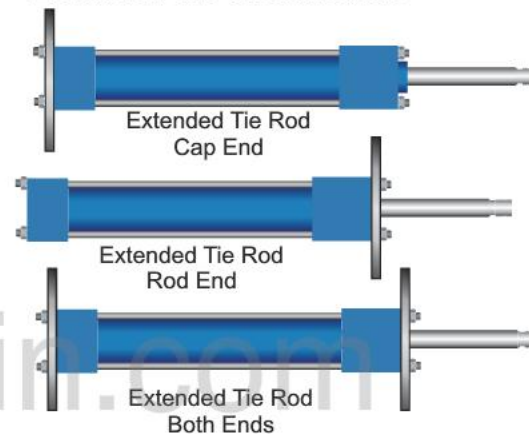


Figure 7-10 Cylinder mounting methods
COPYRIGHT © (2001) EATON CORPORATION

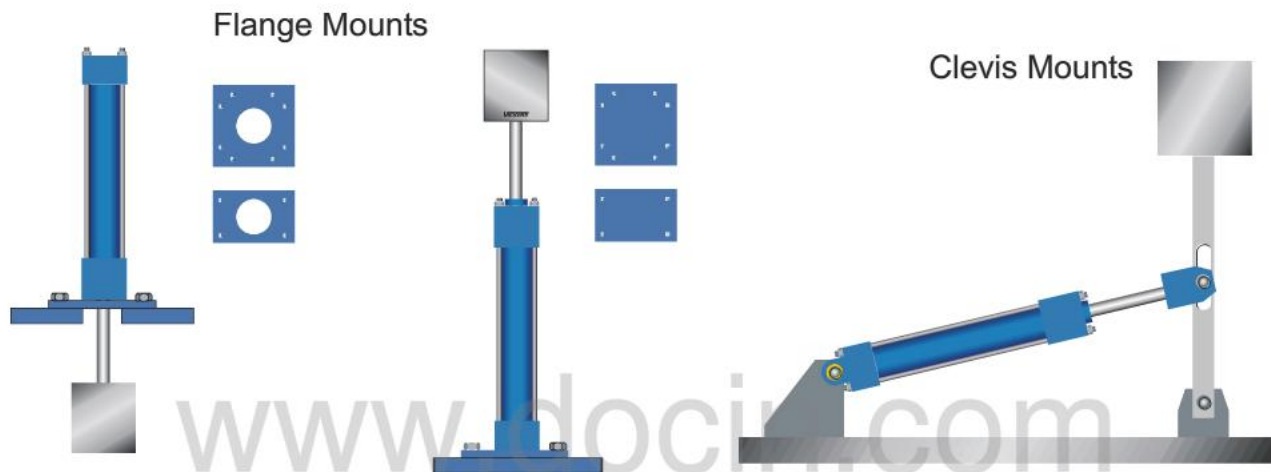


Figure 7-10 Cylinder mounting methods
COPYRIGHT (C) (2001) EATON CORPORATION

Trunnion Mounts

Cap End Trunnion



Rod End Trunnion



Intermediate Trunnion



Figure 7-10 Cylinder mounting methods

COPYRIGHT © (2001) EATON CORPORATION

Change	Speed	Load Pressure	Max Force
Increase relief valve setting	No effect	No effect	Increase
Decrease relief valve setting	No effect	No effect	Decrease
Increase gpm	Increase	No effect	No effect
Decrease gpm	Decrease	No effect	No effect
Increase cylinder diameter	Decrease	Decrease	Increase
Decrease cylinder diameter	Increase	Increase	Decrease

Table 7-1 Summary of effects of application changes on cylinder performance

COPYRIGHT © (2001) EATON CORPORATION

Cyl. Bore Dia. Inch	Piston Rod Dia. Inch	Work Area Square Inch	Hydraulic Working Pressure PSI						Fluid Required per In of Stroke		Port Size Dia Inch	Fluid Velocity @ 15 ft/sec	
			500	750	1000	1500	2000	3000	Gal.	Cubic Inch		Flow gpm	Piston Velocity in/sec
1-	- 5/8 1	1.767	883	1325	1767	2651	3534	5301	.00765	1.767	½	11.0	24.0
		1.460	730	1095	1460	2190	2920	4380	.00632	1.460			29.0
		.982	491	736	982	1473	1964	2946	.00425	.982			43.1
2	- 1 1 3/8	3.141	1571	2356	3141	4711	6283	9423	.01360	3.141	½	11.0	13.5
		2.356	1178	1767	2356	3534	4712	7068	.01020	2.356			18.0
		1.656	828	1242	1656	2484	3312	4968	.00717	1.656			25.6
2-	- 1 1 3/8 1	4.909	2454	3682	4909	7363	9818	14727	.02125	4.909	½	11.0	8.6
		4.124	2062	3093	4124	6186	8248	12372	.01785	4.124			10.3
		3.424	1712	2568	3424	5136	6848	10272	.01482	3.424			12.4
		2.504	1252	1878	2504	3756	5008	7512	.01084	2.504			16.9
3-	- 1 3/8 1 2	8.296	4148	6222	8296	12444	16592	24888	.0359	8.296	¾	20.3	9.4
		6.811	3405	5108	6811	10216	13622	20433	.0295	6.811			11.5
		5.891	2945	4418	5891	8836	11782	17673	.0255	5.891			13.3
		5.154	2577	3865	5154	7731	10308	15462	.0223	5.154			15.2
4	- 1 2 2	12.566	6283	9425	12566	18849	25132	37698	.0544	12.566	¾	20.3	6.2
		10.161	5080	7621	10161	15241	20322	30483	.0440	10.161			7.7
		9.424	4712	7068	9424	14136	18848	28272	.0408	9.424			8.3
		7.657	3828	5743	7657	11485	15314	22978	.0331	7.657			10.2

Table 7-2 Data for various size cylinders

COPYRIGHT © (2001) EATON CORPORATION

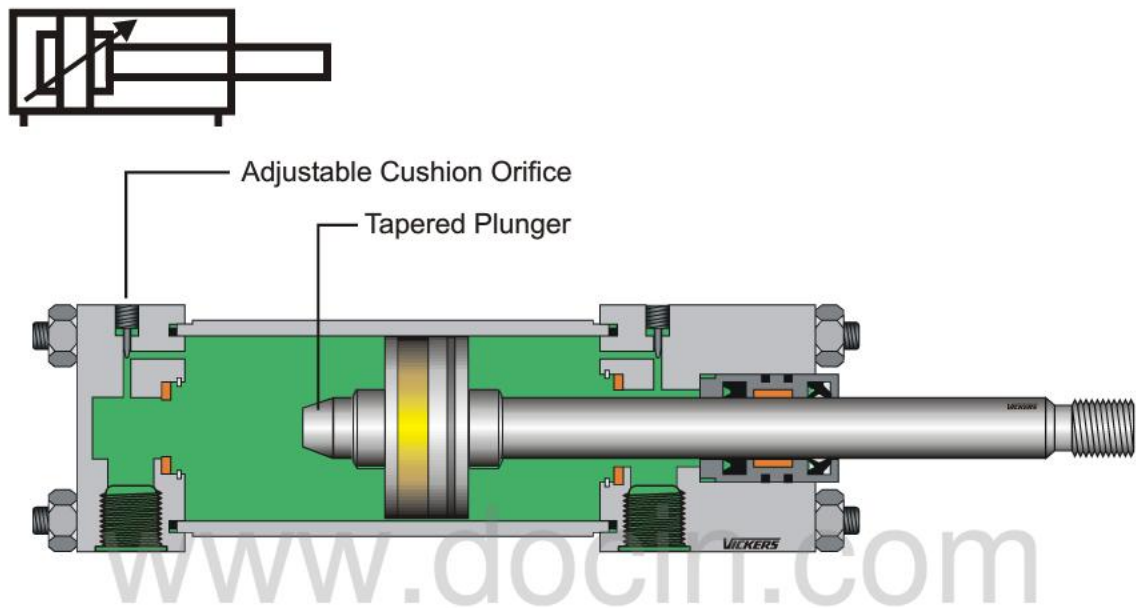


Figure 7-11 Cylinder with extension and retraction cushions

COPYRIGHT © (2001) EATON CORPORATION

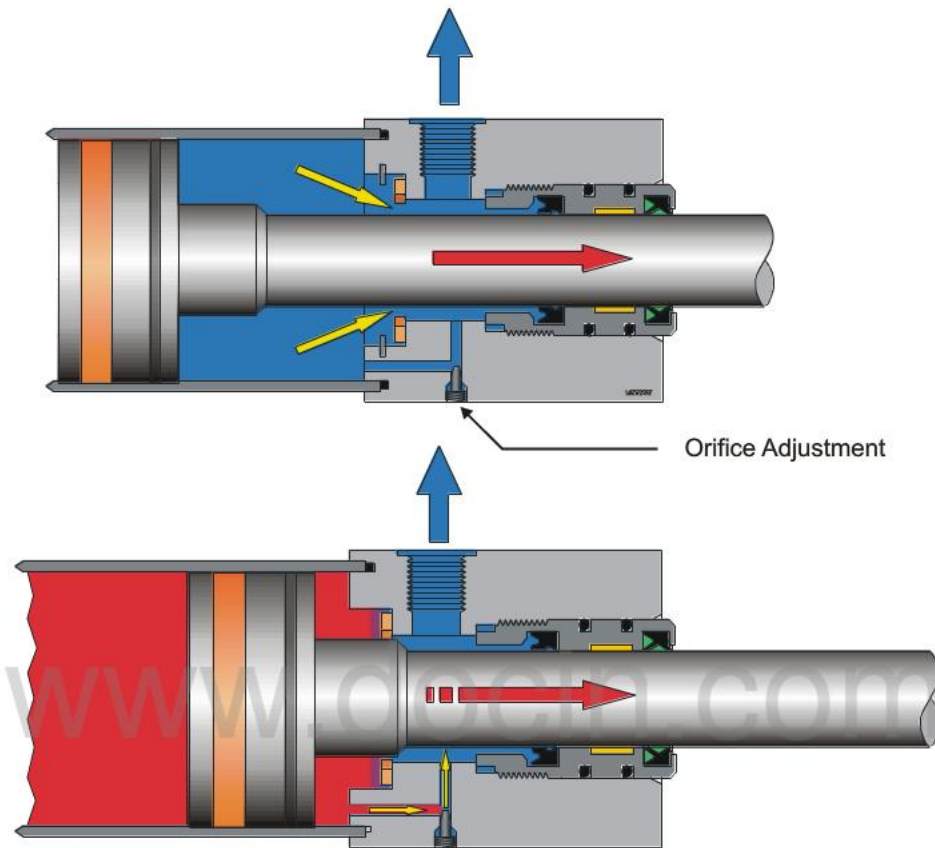


Figure 7-12 Rod end cushion during cylinder extension

COPYRIGHT © (2001) EATON CORPORATION

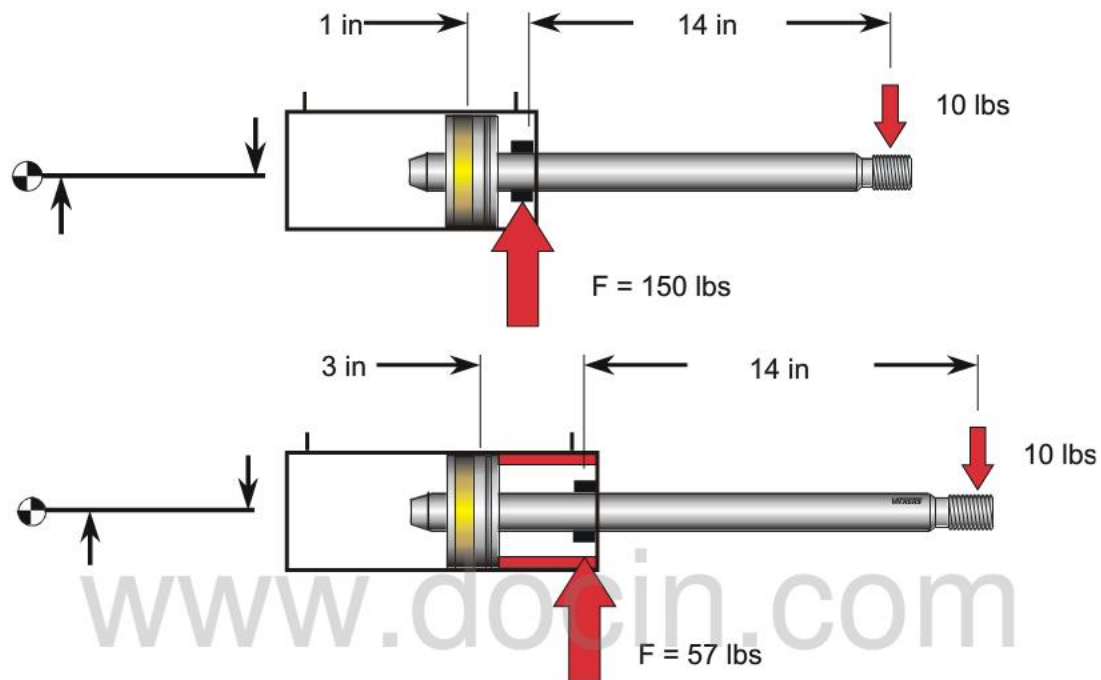


Figure 7-13 A stop tube provides better cylinder rod support

COPYRIGHT © (2001) EATON CORPORATION

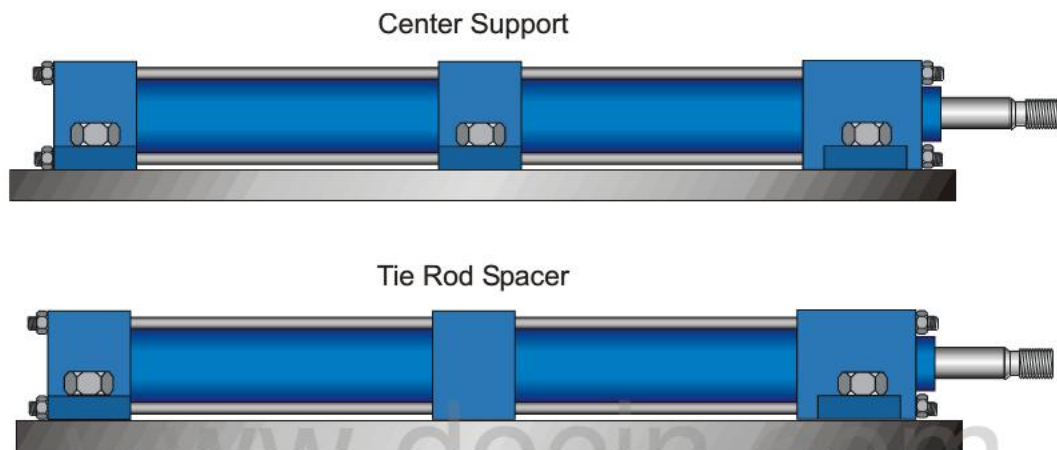


Figure 7-14 Tie rod spacer and center support

COPYRIGHT © (2001) EATON CORPORATION

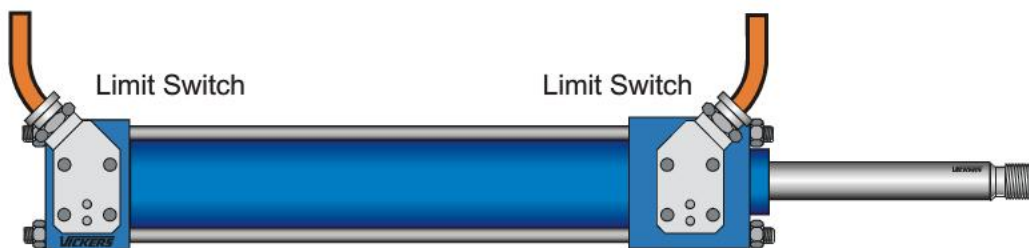


Figure 7-15 Cylinder with limit switches

COPYRIGHT © (2001) EATON CORPORATION

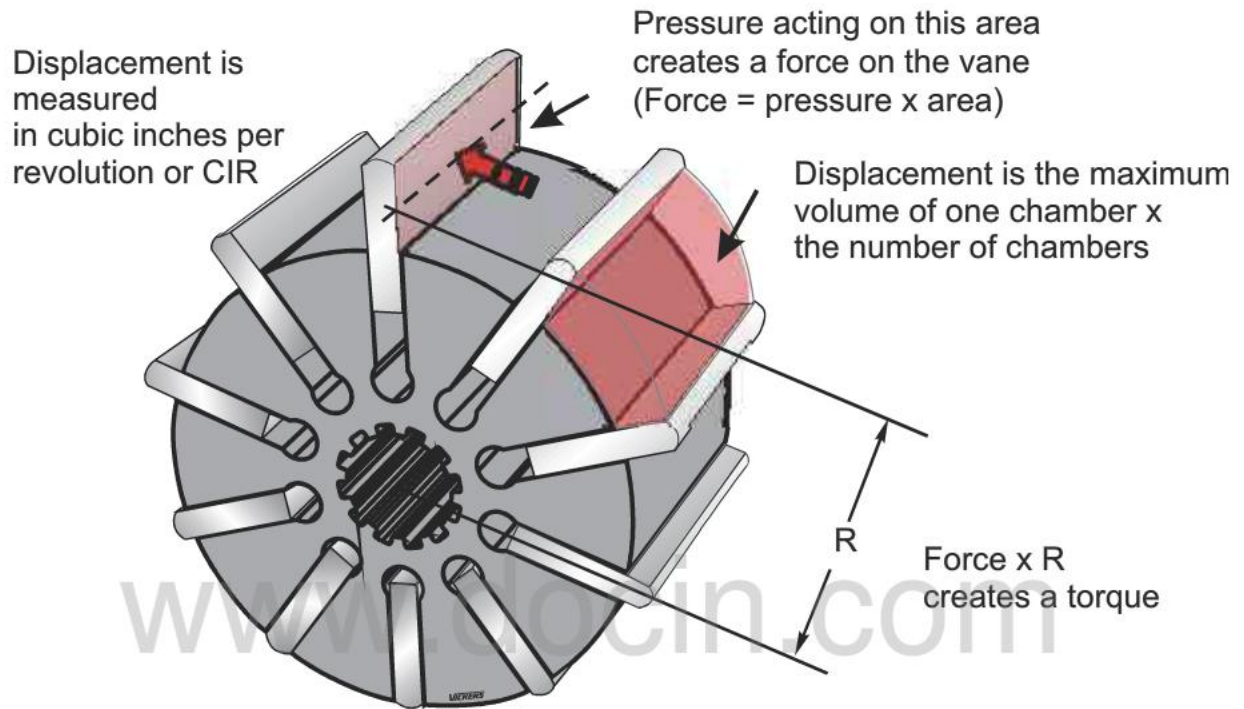


Figure 7-16 Displacement is the quantity of fluid that effects one shaft revolution

COPYRIGHT © (2001) EATON CORPORATION

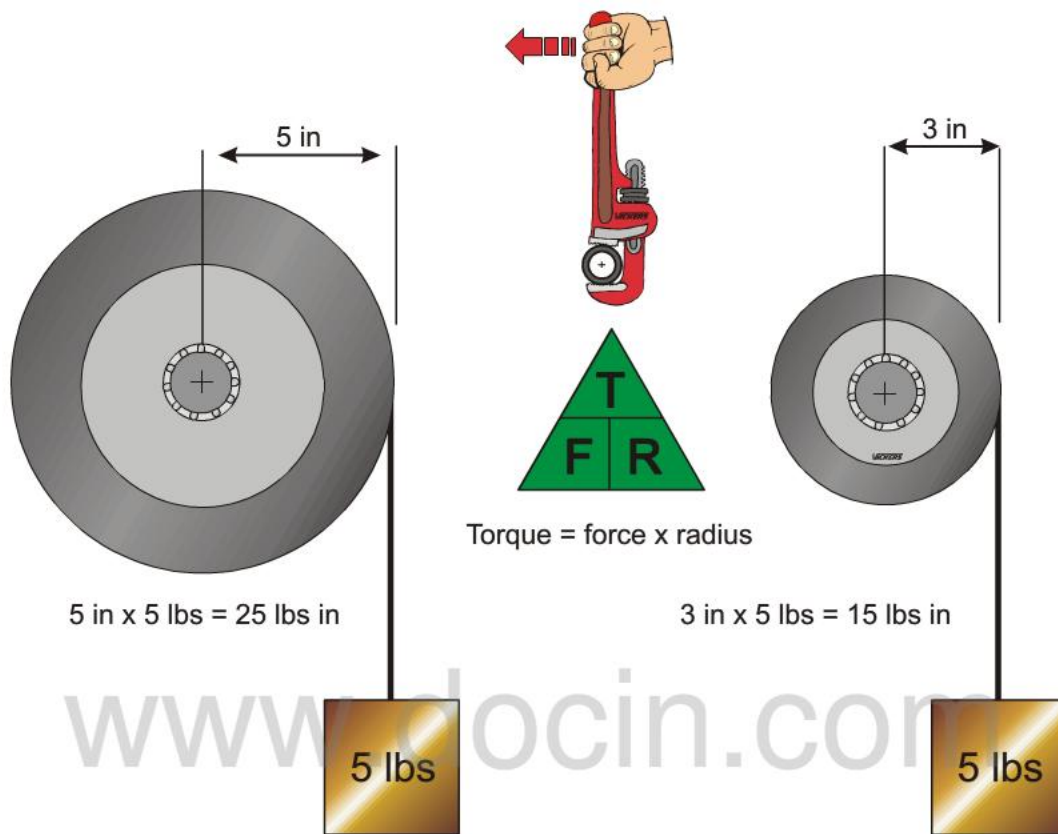
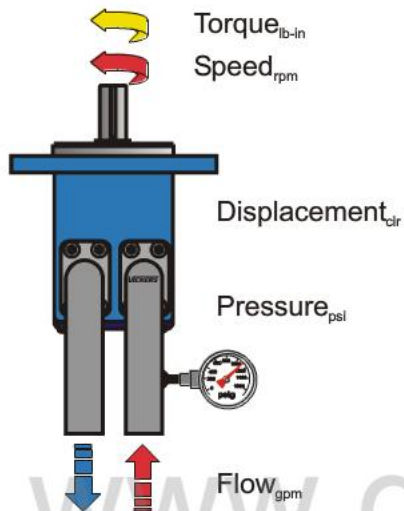


Figure 7-17 Torque equals load multiplied by radius

COPYRIGHT © (2001) EATON CORPORATION

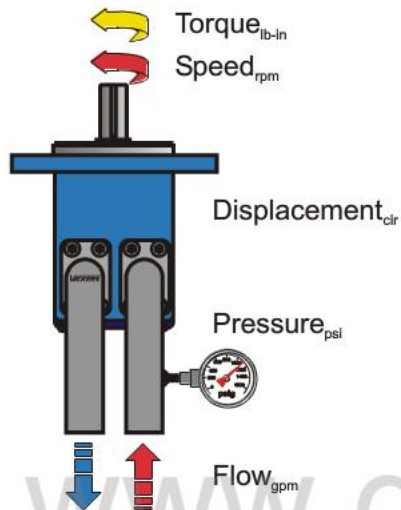


$$\text{Torque}_{\text{lb-in}} = \frac{\text{Pressure}_{\text{psi}} \times \text{Displacement}_{\text{clr}}}{2\pi}$$

$$\text{Pressure}_{\text{psi}} = \frac{\text{Torque}_{\text{lb-in}} \times 2\pi}{\text{Displacement}_{\text{clr}}}$$

Figure 7-18 Hydraulic motor torque formula

COPYRIGHT © (2001) EATON CORPORATION

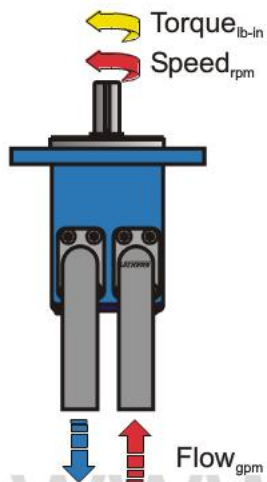


$$\text{Speed}_{\text{rpm}} = \frac{\text{Flow}_{\text{gpm}} \times 231}{\text{Displacement}_{\text{clr}}}$$

$$\text{Flow}_{\text{gpm}} = \frac{\text{Displacement}_{\text{clr}} \times \text{Speed}_{\text{rpm}}}{231}$$

Figure 7-19 Hydraulic motor speed formula

COPYRIGHT © (2001) EATON CORPORATION



$$\text{Horsepower}_{\text{mech}} = \frac{\text{Torque}_{\text{lb-in}} \times \text{Speed}_{\text{rpm}}}{63025}$$

$$\text{Horsepower}_{\text{mech}} = \frac{\text{Torque}_{\text{lb-ft}} \times \text{Speed}_{\text{rpm}}}{5252}$$

Figure 7-20 Hydraulic motor horsepower formula

COPYRIGHT © (2001) EATON CORPORATION

Change	Speed	Load Pressure	Max Torque
Increase relief valve setting	No effect	No effect	Increase
Decrease relief valve setting	No effect	No effect	Decrease
Increase gpm	Increase	No effect	No effect
Decrease gpm	Decrease	No effect	No effect
Increase displacement cir	Decrease	Decrease	Increase
Decrease displacement cir	Increase	Increase	Decrease

Table 7-3 Summary of effects of application changes on motor operations

COPYRIGHT © (2001) EATON CORPORATION

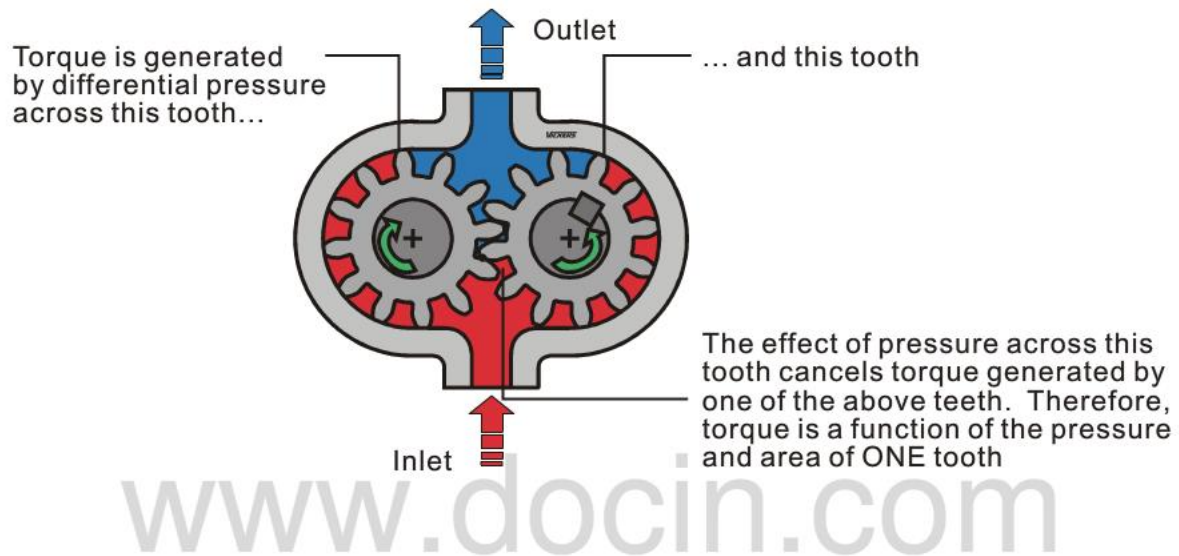


Figure 7-21 Torque generation in an external gear motor

COPYRIGHT © (2001) EATON CORPORATION

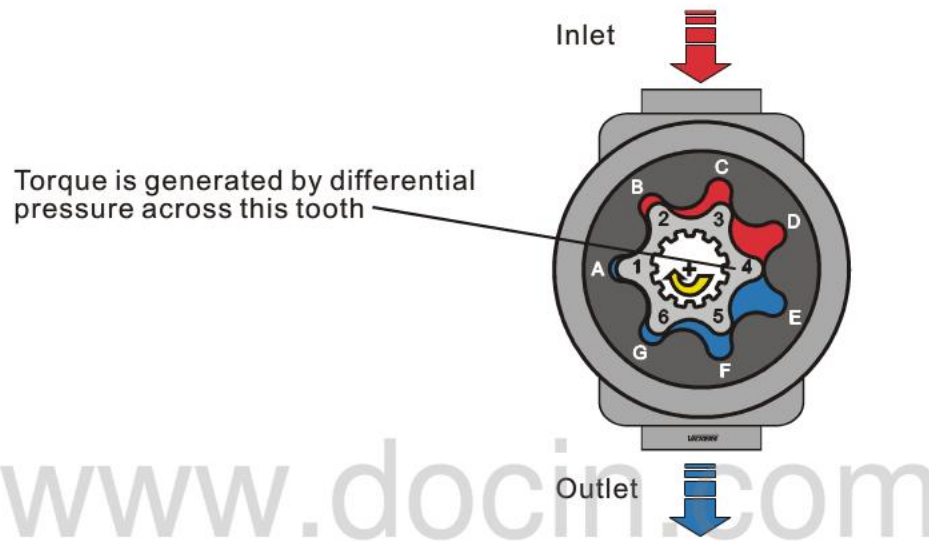


Figure 7-22 Cross section of a direct drive gerotor motor

COPYRIGHT © (2001) EATON CORPORATION

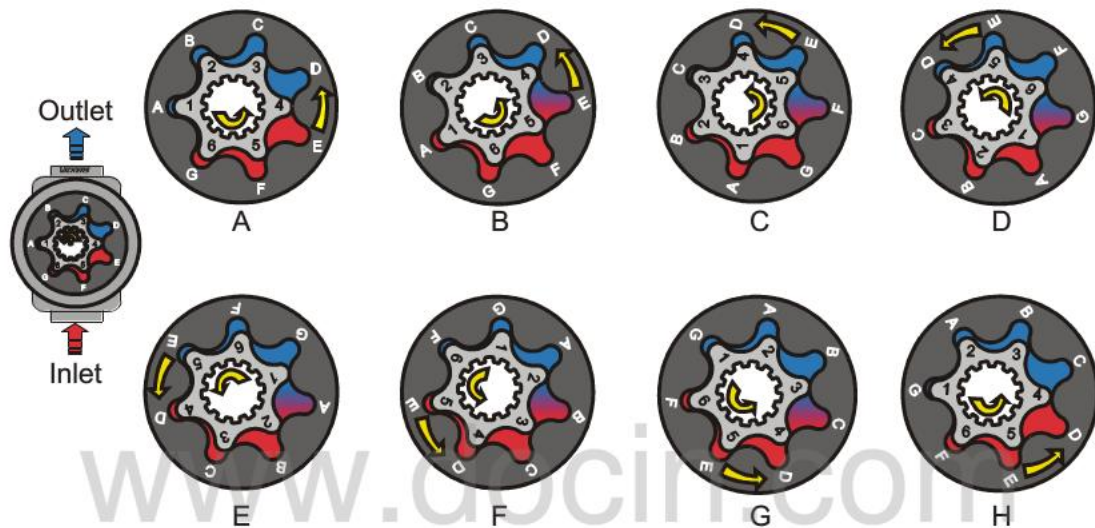


Figure 7-23 Sequence of direct drive gerotor motor

COPYRIGHT © (2001) VICKERS, INCORPORATED

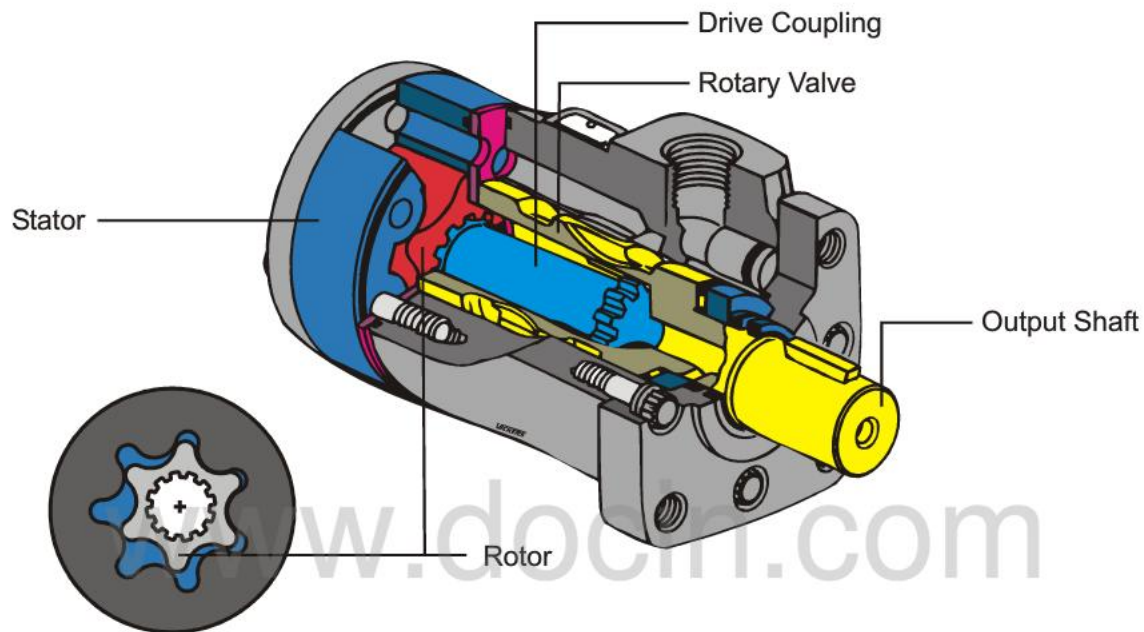


Figure 7-24 An orbiting gerotor motor

COPYRIGHT © (2001) EATON CORPORATION

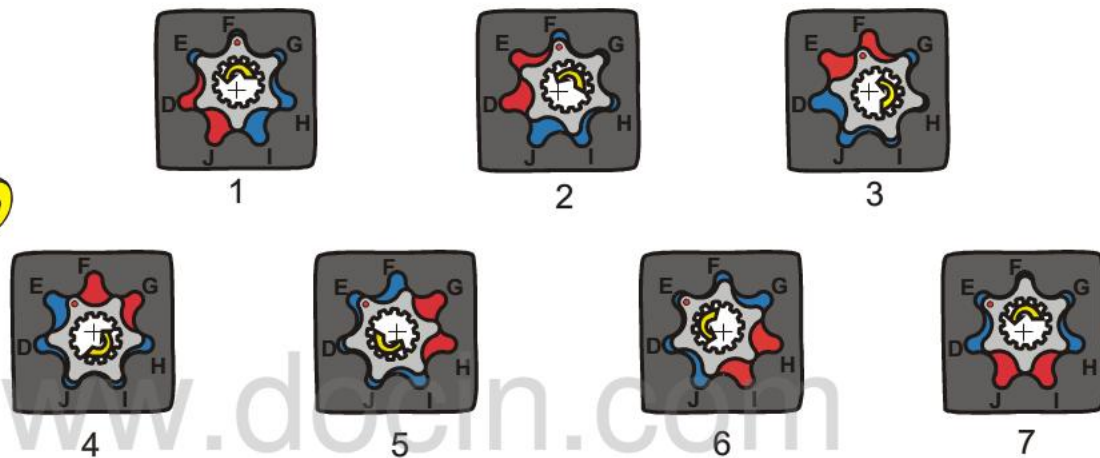
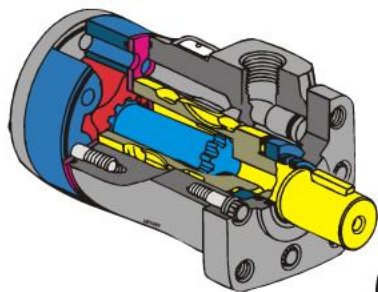


Figure 7-25 Sequence of an orbiting gerotor motor

COPYRIGHT © (2001) EATON CORPORATION

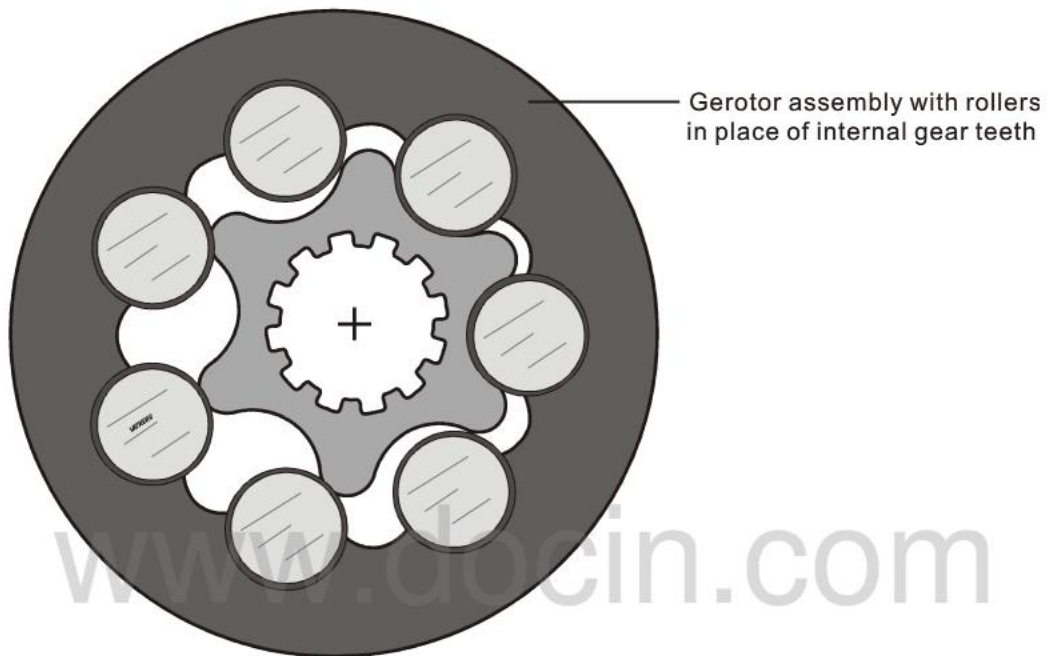


Figure 7.26 Roller-vane gerotor motor

COPYRIGHT © (2001) EATON CORPORATION

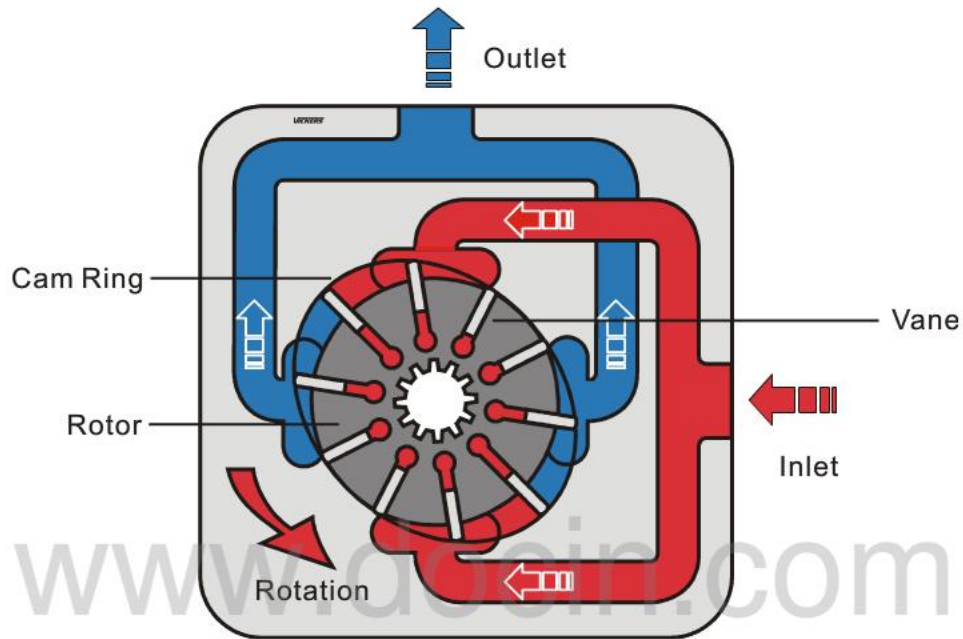


Figure 7-27 Cross section of a balanced vane motor rotating group

COPYRIGHT © (2001) EATON CORPORATION

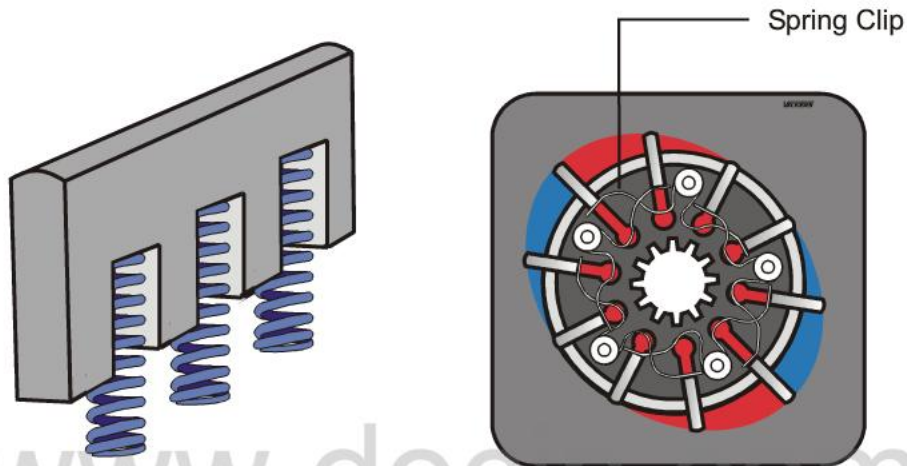


Figure 7-28 Springs or spring clips keep the vanes against the cam

COPYRIGHT © (2001) EATON CORPORATION

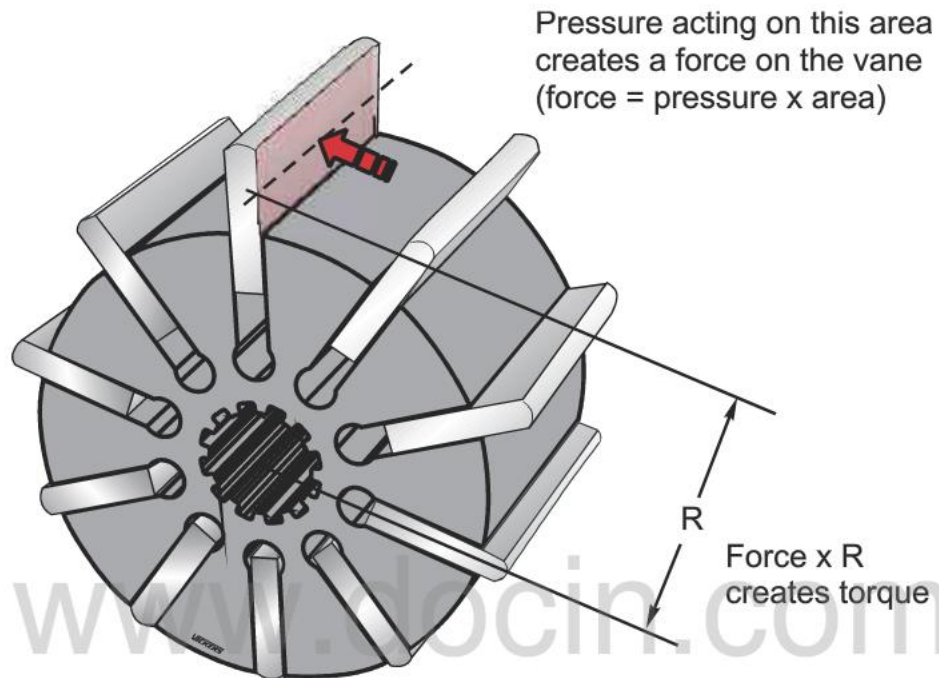


Figure 7-29 Pressure acting on a vane creates torque on the drive shaft

COPYRIGHT © (2001) EATON CORPORATION

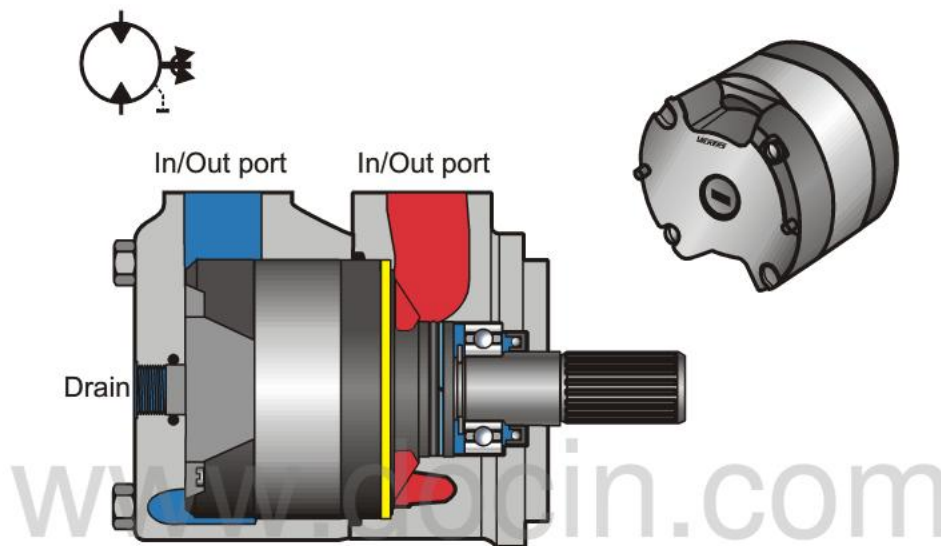


Figure 7-30 High performance vane motor cartridge design

COPYRIGHT © (2001) EATON CORPORATION

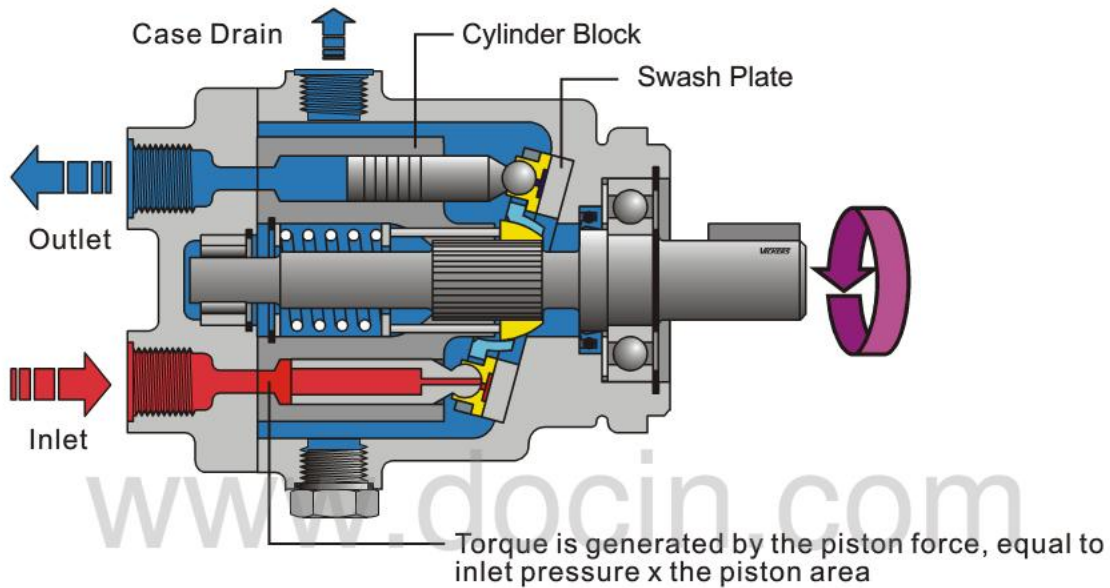


Figure 7-31 Fixed displacement in-line piston motor

COPYRIGHT © (2001) EATON CORPORATION

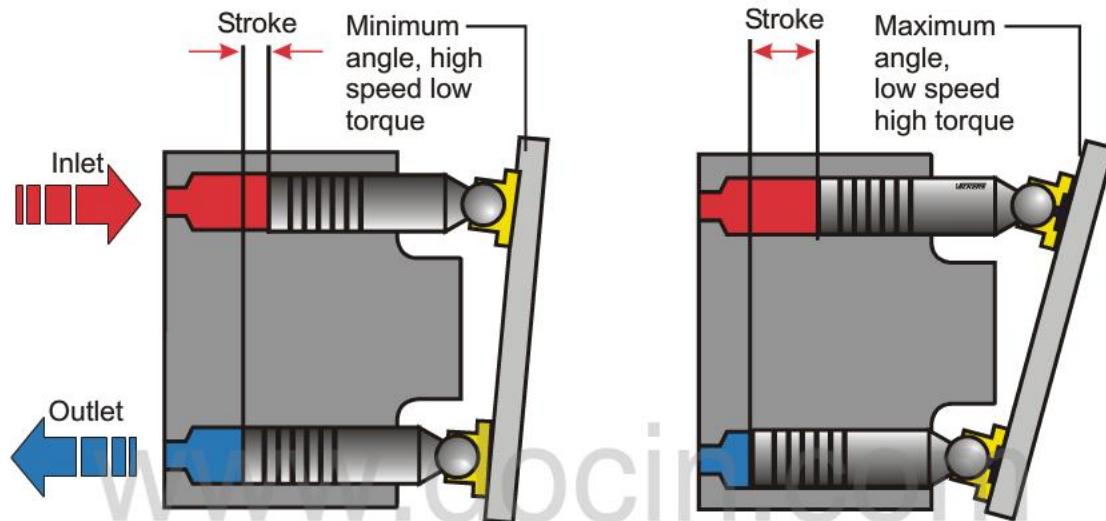


Figure 7-32 Swash plate angle determines the torque and speed relationship

COPYRIGHT © (2001) EATON CORPORATION

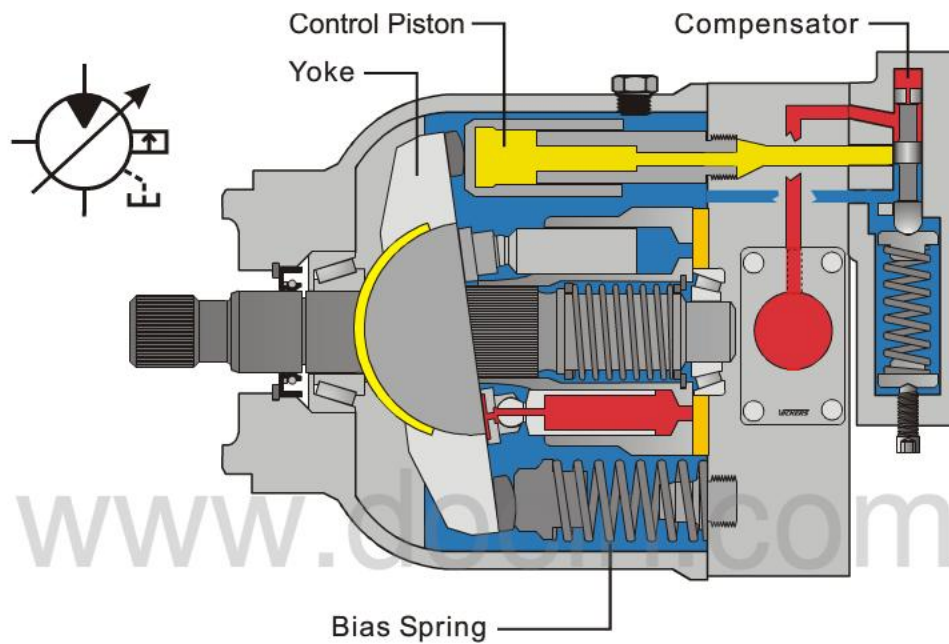


Figure 7-33 Variable displacement in-line piston motor

COPYRIGHT © (2001) EATON CORPORATION

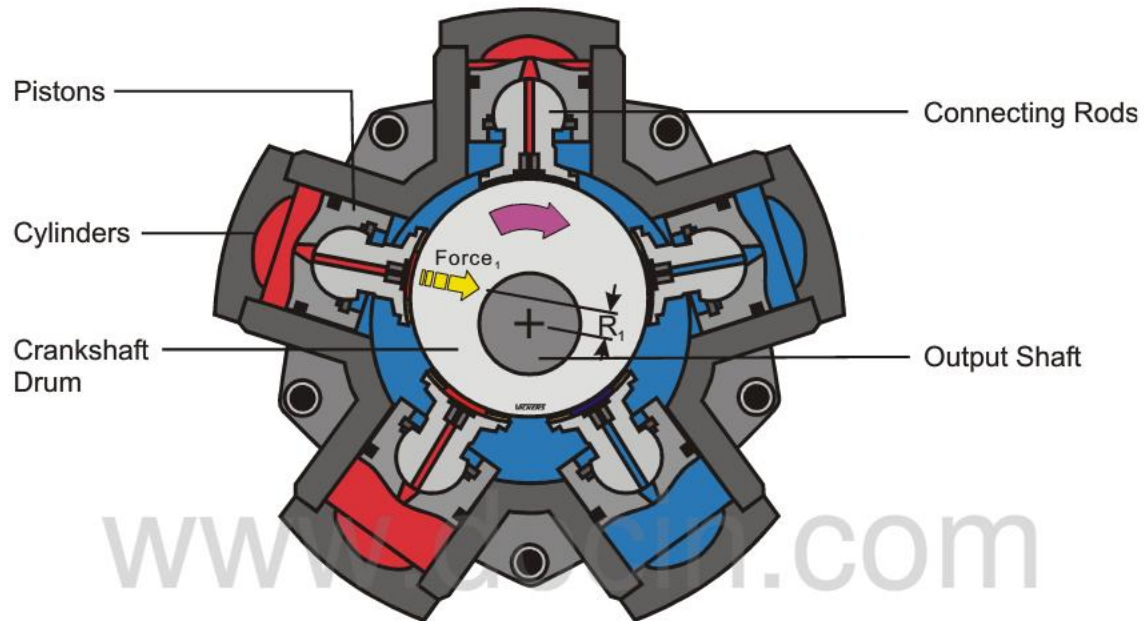


Figure 7-34 Radial piston motor

COPYRIGHT © (2001) EATON CORPORATION

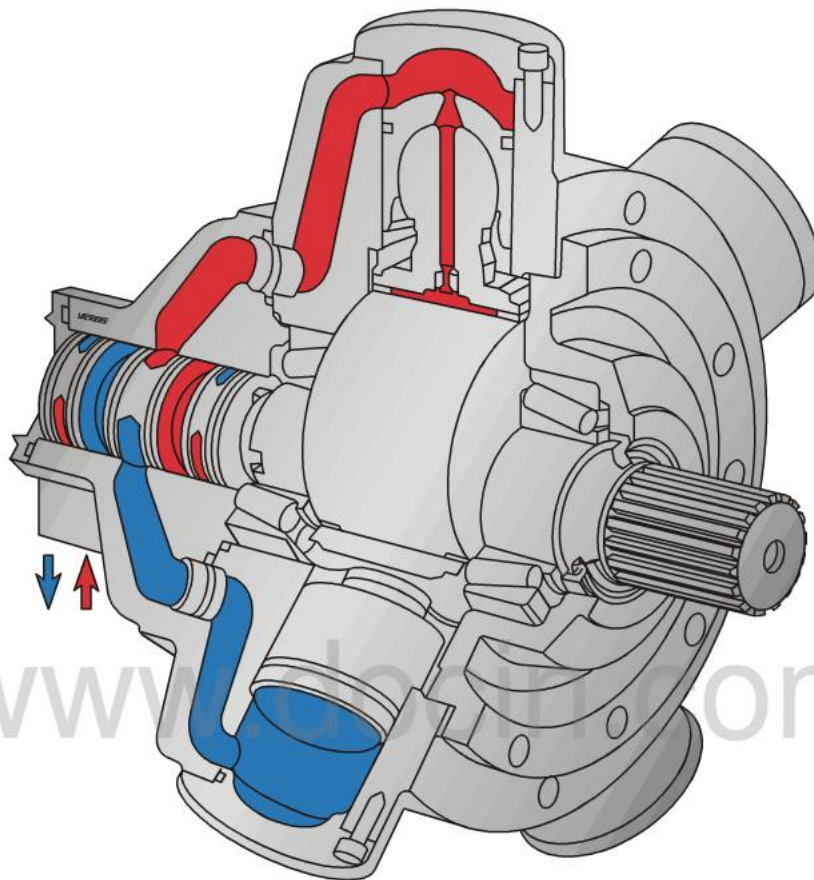


Figure 7-35 Inlet and outlet porting in a radial piston motor

COPYRIGHT © (2001) EATON CORPORATION

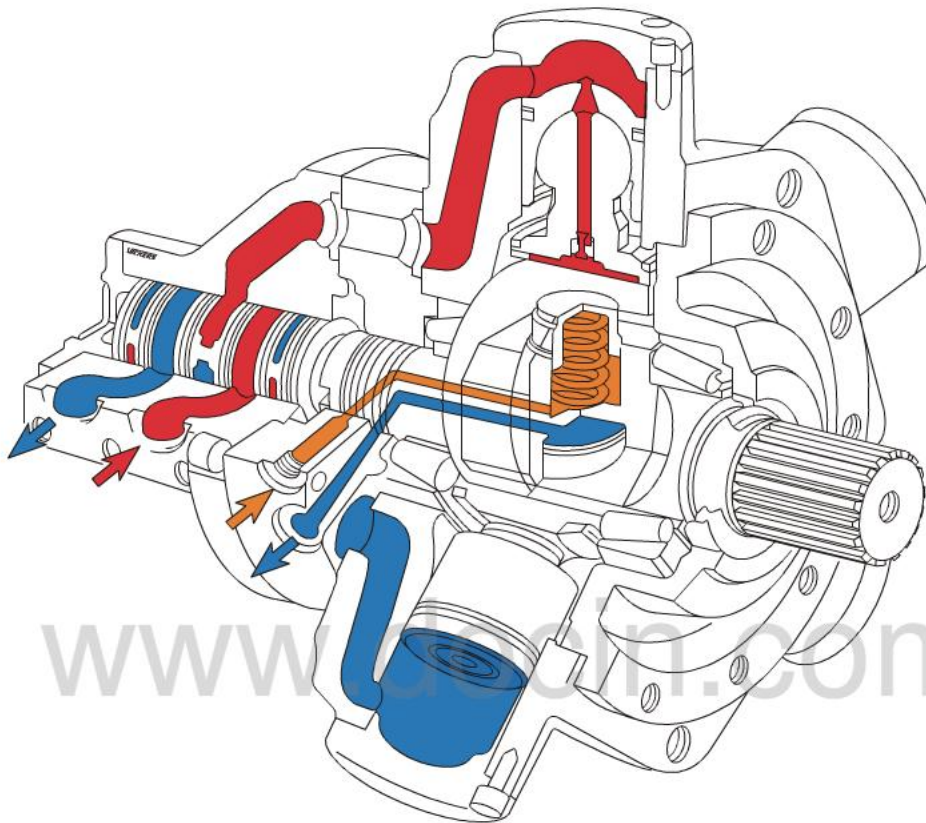


Figure 7-36 Variable displacement radial piston motor

COPYRIGHT © (2001) EATON CORPORATION

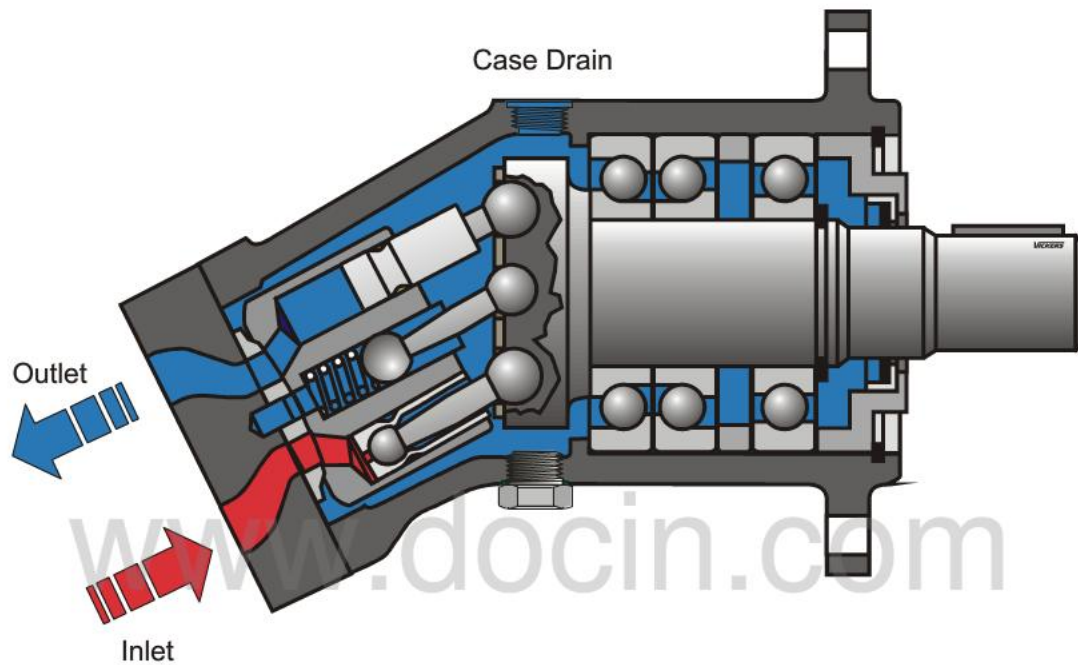


Figure 7-37 Bent axis piston motor

COPYRIGHT © (2001) EATON CORPORATION

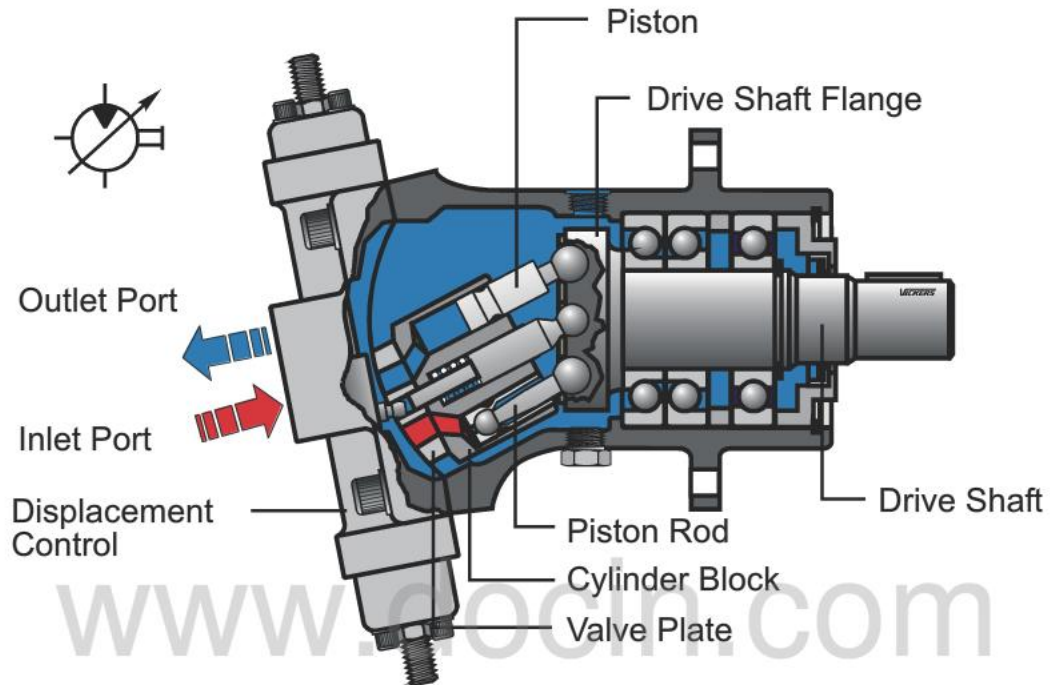


Figure 7-38 Variable displacement bent axis piston motor

COPYRIGHT © (2001) EATON CORPORATION

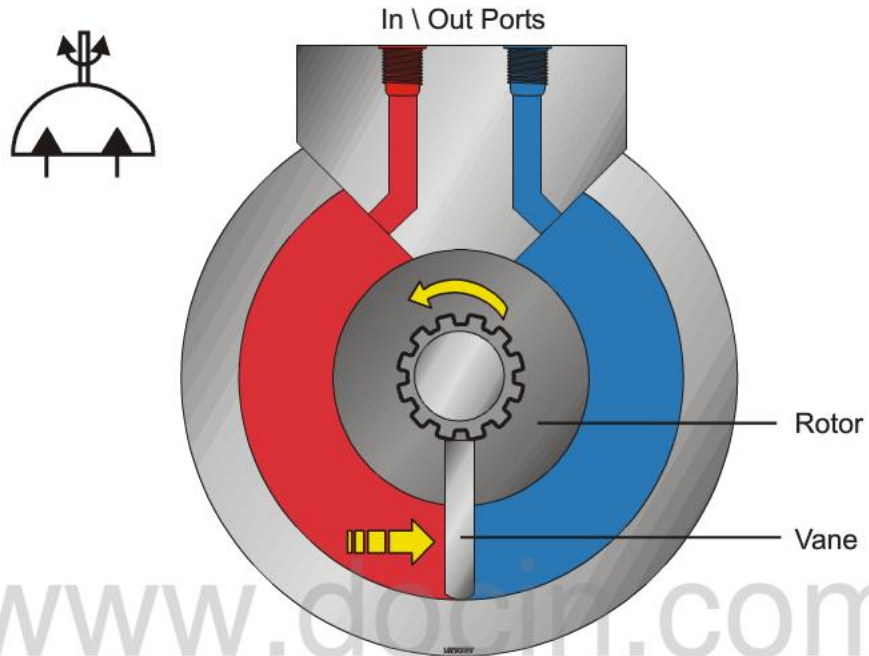


Figure 7-39 Limited rotation actuator

COPYRIGHT © (2001) EATON CORPORATION